



Calibration of HY-2A Satellite Scatterometer with Ocean and Considerations of Calibration of CFOSAT Scatterometer

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Nese CFOSAT SCAT Mission Updates

- CFOSAT (Chinese-French Oceanic SATellite) is a China-France jointly developed oceanic satellite, CFOSAT has two radar payloads:
- Ku-band real aperture radar for measurement of directional ocean surface wave measurement (SWIM).
- Ku-band radar scattermeter (SCAT) for ocean surface wind vector measurement;



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Milestones of CFOSAT SCAT



- Apr, 2010, Preliminary design review;
- Dec, 2010, Detailed design review;
- Jul, 2011, Satellite interface compatibility test and SCAT electrical performance test;
- Nov, 2011, Delivery of mechanical and thermal models;
- Oct, 2012, Airborne validation experiments at Yellow Sea, China.
- Jun, 2013, Environmental experiments
- Feb, 2014, Delivery of electrical models
- Apr, 2014, CFOSAT RM2/EMC Test
- 2018, Launch.

Airborne Validation Experiments

- To Validate the SCAT system design and reliability;
- Using all the instruments of the spaceborne scatterometer to except the power amplifier and the antenna.
- Software of SCAT is redesigned due to observation geometry of airborne platform.







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Airborne Validation Experiments

Test Results of Airborne Scatterometer







Retrieval Results Compared with real time wind vectors and HY-2A Scatterometer

Date	Airborne Scatterometer	HY-2A Scatterometer	Real time wind vectors (Measured on ships)	Wind Vector Errors
2012-11-2	4.8 m/s@28°	5.6 m/s@43°	5.0 m/s@30 $^{\circ}$	0.2 m/s@2°
2012-11-7	3.4 m/s@104 $^\circ$	-	$3.5~\mathrm{m/s}@112^\circ$	0.1 m/s@8°
2012-11-8	4.3 m/s@174 $^{\circ}$	5.0 m/s@141 $^\circ$	4.8 m/s@168°	0.5 m/s@6°
2012-11-12	11.0 m/s @105 $^\circ$	-	11.6 m/s @112 $^\circ$	0.6m/s @7°
2012-11-14	6.4 m/s @159 $^\circ$	6.1 m/s @175 $^{\circ}$	7.1 m/s @177 $^\circ$	0.7 m/s @18 $^{\circ}$
2012-11-17	11.0 m/s @124 $^\circ$	-	11.5 m/s @135 $^\circ$	$0.5 \mathrm{m/s}@11^{\circ}$





Environmental Experiments

Random Vibration, Sine Vibration and Shock Tests







Environmental Experiments

Thermal Test and Thermal Vacuum Tests







Environmental Experiments

The Calibration signal and Internal Noise during thermal test (one cycle)



Calibration signal changes at different temperatures

Internal Noise changes at different temperatures







CFOSAT RM2/EMC Test

Satellite configuration in the EMC chamber



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Internal Calibration

- --Fluctuations of Tx power and Rx gain
- --Fluctuations of Rx noise level
- --Fluctuations of Rx transfer characteristics
- External Calibration
- --In-orbit antenan gain pattern, especially the elevation part
 --Fluctuations of insert loss during the antenna rotation
 --Satellite attitude errors







--The programmable gain controller inside the receiver has a repetitive precision of 0.1dB ; --The measurement precisions for passive part of the transmitting/receiveing channel are both less than 0.05dB;

--The clutter by coupling outside the calibration loop is more than 20dB lower than the power coupled from the internal calibration loop, which leads to uncertainty of about 0.05dB.

--The fluctuation of the insertion loss of the rotary joint has a residual of less than 0.05dB;

The overall internal calibration error is better than 0.15dB





External Calibration

Purpose:

- --Calibration of in-orbit antenna pattern;
- --Calibration of fluctuations of insert loss of rotary joint
- --Estimation of satellite attitude errors

Possible Solutions:

- --Natural area-extended target with uniform Sigma-0
- --Calibration ground stations
- --NOC will be used to improve the wind retrieval quality





Several homogenenous areas over land are analyzed.(2009 QuikSCAT SIR)







Several homogenenous areas over land are analyzed using HY-2 L1B data

Region	Pass	VV Polarization		HH Polarization	
		Average	Std Dev	Average	Std Dev
		(dB)		(dB)	
Amazon	Asc	-8.35	0.43	-7.67	0.41
	Des	-8.14	0.40	-7.29	0.42
Congo	Asc	-8.34	0.43	-7.94	0.43
	Des	-7.94	0.39	-7.38	0.41
Antarctic	Asc	-5.55	0.40	-5.65	0.40
	Des	-5.47	0.39	-5.66	0.41
Greenland	Asc	-5.20	0.39	-5.83	0.36
	Des	-5.14	0.30	-5.64	0.36
Sahara	Asc	-22.48	0.84	-21.57	0.85
	Des	-22.53	0.87	-21.58	0.90





Models:
$$\sigma_{\text{meas,n}}^{0}(\text{dB}) = \sigma_{\text{tr}}^{0}(L_{n},\theta_{n},\text{Asc/Des}) + \Delta \sigma_{G}^{0}(L_{n},b_{n},t_{n},\text{Asc/Des}) + \Delta \sigma_{\text{noise}}^{0}$$

 $\Delta \sigma_{abs}^{0} + \Delta \sigma_{r}^{0}$
 \Rightarrow speed direction
 $\sigma_{\text{meas,n}}^{0} = \sigma_{\text{eff}}^{0}(\theta_{n}) + \Delta \sigma_{r}^{0}(b_{n},\theta_{n})$

fourth order polynomial fitting (Long, Skouson, *TGRS*, 1996) $\sigma_{\text{meas}}^{0} = c(0,k) + c(1,k)\theta_{n} + c(2,k)\theta_{n}^{2} + c(3,k)\theta_{n}^{3} + c(4,k)\theta_{n}^{4}$

 $c(i,k) = c_{\text{eff}}(i,k) + c_r(i,k)$

In order to characterize the azimuthal-dependent bias (mainly casued by the rotary joint), the azimuth angles of the antenna beam are separated into 24 bins, which are sufficient for correcting the expected relative bias.





Simulation Results (STD<0.1dB)







Satellite attitude $F_1(\theta_r, \theta_y, \theta_p) = \frac{1}{N} \sum_{i=1}^{N_m} (G_{\text{MEAS}}(\theta_N(i), \varphi_N(i)) - G_{\text{NOM}}(\theta_{\text{ACT}}(i), \varphi_{\text{ACT}}(i)))^2 \text{Observation geometry}_{\text{Instrument parameters}}$ Instrument parameters Antenna gain pattern $F_2(c_{\rm nm}) = \frac{1}{N} \sum_{k=1}^{N_m} \left(G_{\rm MEAS}(\theta_N, \varphi_N) - G_{\rm NOM}(\theta_N, \varphi_N, \theta_r^{est}, \theta_y^{est}, \theta_p^{est}) - G_{\rm DIS} \right)^2 \left| \begin{array}{c} {\rm RFSCAT \ Calibration} \\ {\rm Simulation \ model} \end{array} \right|^2$ Simulated CGS data $RMS = \sqrt{\frac{1}{N_m} \sum_{i=1}^{N_m} \left(G_{MEAS} \left(\theta_N \left(i \right), \varphi_N \left(i \right) \right) - G_{MODEL} \left(\theta_N \left(i \right), \varphi_N \left(i \right) \right) \right)^2}$ Comparion Satellite attitude errors RFSCAT Calibration Actual CGS Fluctuations of insert loss of rotary joint Simulation model measured data $F_{3}(d_{k}) = \frac{1}{N} \sum_{i=1}^{N_{m}} \left(G_{\text{DIF}}(i) - \sum_{i=1}^{N} d_{k} \phi^{k}(i) \right)^{2}$ Simulated CGS data $G_{\text{DIF}} = G_{\text{MEAS}}\left(\theta_{N}, \varphi_{N}\right) - G_{\text{NOM}}\left(\theta_{N}, \varphi_{N}, \theta_{r}^{est}, \theta_{v}^{est}, \theta_{p}^{est}\right)$ Comparion $-\sum \sum c_{nm} \theta^m_{ACT} \varphi^n_{ACT}$ The variation of т antenna gain



Considertions of Calibration of CFOSAT SCAT





Considertions of Calibration of CFOSAT SCAT



The STD of **yaw** angle estimation is<0.01deg

The estimation result of the loss due to rotary joint(STD<0.05dB)





Simulation Results of CGS

CAL	RFSCAT	CGS	Estimation error of Attitude(deg)			Rotary joint	Antenna	
Window	Work		Pointing	Roll	Yaw	Pitch	loss (dB)	gain(dB)
	mode		error					
	Normal	T ₁	0.005	0.002	0.008	0.003	0.08	0.12
13 day	mode	T ₂	0.004	0.001	0.007	0.002	0.04	0.10
		T_1+T_2	0.004	0.001	0.007	0.002	0.05	0.09
	Only VV	T ₁	0.005	0.002	0.008	0.003	0.09	0.16
13 day	or HH	T ₂	0.004	0.001	0.007	0.002	0.04	0.11
	mode	T_1+T_2	0.004	0.001	0.007	0.002	0.05	0.09
	Normal	T ₁	0.005	0.001	0.008	0.002	0.05	0.11
26 day	mode	T ₂	0.004	0.001	0.007	0.002	0.05	0.06
		T_1+T_2	0.004	0.001	0.007	0.001	0.05	0.06

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Simulation Results of CGS

 $\Delta \theta_{\text{point}} = \sqrt{\left(\Delta \theta_r\right)^2 + \left(\Delta \theta_y\right)^2 + \left(\Delta \theta_p\right)^2}$

 $10\log_{10}\left(1+\frac{\Delta G_{\text{slant}}}{G}\right) = 10\log_{10}\left(1+\frac{2\Delta R}{R}\right)$



Less than 0.05dB

The slant range to the near swath edge for the SCAT on CFOSAT is always greater than 570km. The bias error (100m) of slant range introduced into angenna gain error will be less than 0.0015dB

Atmospheric loss would be mainly related with oxygen content and water vapor density in the Clear sky. It would be reasonable to assume that one-way loss in the loss is about 0.0065dB/km under the condition that relative humidity is 30% lower. The variation of atmospheric loss after compensation is about 0.04dB

$$\Delta \sigma_{\text{scat}}^{0} = \sqrt{\left(\Delta \sigma_{\text{point}}^{0}\right)^{2} + \left(\Delta \sigma_{\text{DIS}}^{0}\right)^{2} + \left(\Delta \sigma_{L}^{0}\right)^{2} + \left(\Delta \sigma_{\text{slant}}^{0}\right)^{2} + \left(\Delta \sigma_{\text{cGS}}^{0}\right)^{2} + \left(\Delta \sigma_{\text{atm}}^{0}\right)^{2}} \qquad \text{Less than } 0.2 \text{dB}$$

Se Considertions of Calibration of CFOSAT SCAT



NWP Ocean Calibration (NOC):

Signals are averaged into 15 km spaced slice along-elevation. A slice can be regarded a special pencil-beam. Thus, rotating Fanbeam scatterometer can be divided into a combinations of series rotating pencil-beam. The NOC technique used for rotating pencil-beam scatterometer will be adopted for the calibration of RFSCAT.



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Calibration of HY-2A SCAT

NWP Ocean Calibration (NOC) Stoffelen, J. Atm. Ocean. Tech. 1999
NOC may be applied over a large portion of the globe and consequently Provide accurate results over a relatively short period.
NOC has been applied successfully for the calibration of ASCAT and OSCAT at KNMI.

Dataset:

--L2A: December 1-31, 2012, 25km resolution 76WVC provided by NSOAS
--L2B: processed at NSSC using OWDP NWP Winds:ECMWF NWP equivalent neutral winds
Globe buoys data
GMF: NSCAT-3





Calibration of HY-2A SCAT

December 1-7 2012 NOC correction coefficients December 2012 Residual after NOC





HY-2A SCAT CALIBRATION RESULTS

December 2012 L2B after NOC vs ECMWF





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December 2012 L2B after NOC vs ECMWF







HY-2A SCAT CALIBRATION RESULTS

400 300 Count 200100 0 10 15 25 0 5 20 3 HSCAT bias(m/s) 2 1.5 std dev.(m/s) 0 5 -1 0 5 10 15 20 25 Average Buoy/HSCAT wind speed(m/s)



80°N

60°N

40°N



	collocation	Speed	Speed	Direction	Wind
		bias(m/s)	STD(m/s)	STD(deg)	vector
					STD(m/s)
No corr	3112	1.93	1.93	18.40	4.64
NOC	3112	0.17	1.23	14.88	2.93
corr					

H H

50°E

100°E

150°E

December 2012 L2B after NOC vs Buoys







Thanks for your attention!

